

Nitrogen-enriched Heterocyclic Poly(ionic liquid)s/MXene Composite Membranes for Efficient Dye Separation

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Electronic Supplementary Information

Abstract Organic dyes, as a typical class of persistent pollutants in aquatic environments, pose potential threats to ecosystem safety and public health. Poly(ionic liquid)s (PILs) can provide charge repulsion and MXene can offer interlayer nanochannels, making them ideal candidates for fabricating high-efficiency separation membranes. In this study, composite membrane materials with asymmetric and symmetric structures were facilely constructed by loading coatings of PILs-modified two-dimensional transition metal carbides (MXene, Ti_2C) at various loadings onto polypropylene microfiltration membranes, overcoming the drawbacks of poor stability of pure PIL membranes and severe interlayer stacking of neat MXene membranes, with the aim of achieving efficient separation of dye molecules. Methyl orange, methyl red, methylene blue, and rhodamine B were selected as model dyes to systematically evaluate the separation performance of the as-prepared composite membranes. The results showed that the PILs/MXene composite membranes exhibited excellent rejection performance for the four model dyes, with rejection rates exceeding 99% at higher loading levels (e.g., AM-3/SM-3) while maintaining a high water flux (up to $58.36 \text{ L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{MPa}^{-1}$). The charge interaction between dyes and the membrane surface, as well as the size effect of dye molecules, were key factors that significantly affected the rejection efficiency of the membranes. In addition, the composite membrane displayed favorable operational stability in aqueous environments, demonstrating its application potential in the purification of industrial dye wastewater. This work provides new insights for the development of PILs/MXene composite membranes for dye wastewater purification, meanwhile, the simple membrane fabrication method also endows it with considerable potential for industrial scale-up.

Keywords Porous polymers; Poly(ionic liquid)s; MXene; Composite membrane; Dye separation

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INTRODUCTION

Dye wastewater pollution from textile dyeing, papermaking and other chemical production processes has emerged as a serious environmental and health crisis,^[1] posing persistent toxicity and significant risks to human health and aquatic life.^[2] This can be addressed by removing these dyes from wastewater before they are discharged into the environment^[3].

Various treatment methods, including chemical oxidation,^[4] photocatalysis,^[5] and electrocoagulation,^[6] have been widely used to mitigate the adverse effects of dye wastewater. However, they are often pH-dependent, costly, and may produce unwanted byproducts.^[7] In contrast, membrane separation technology selectively separates components without requiring phase change,^[8] which also occupies

minimal space, has low energy consumption, is cost-effective, and features low carbon emissions, giving it broader application potential in dye separation.^[9] Lee *et al.* explored a coagulation-adsorption-microfiltration submerged membrane system to achieve efficient dye removal from dye wastewater and regenerated water production.^[10]

Poly(ionic liquid)s (PILs) combine the dimensional stability and mechanical durability of polymers with the high ionic conductivity and tunable hydrophilicity and hydrophobicity properties of ionic liquids.^[11] The chemical structure and properties of PIL-based membrane materials can be easily adjusted through simple anion exchange.^[12] Meanwhile, the superior antibacterial activity of PILs renders them well suited for dye wastewater environments, which are prone to bacterial growth.^[13] However, PILs tend to dissolve during phase separation preparation and application, leading to material loss and reduced membrane lifespan.^[14] In addition, PILs typically lack stable porous structures, resulting in low permeability.

Recent advances in 2D materials, including intrinsically layered materials (e.g., graphene oxide (GO))^[15] and MXenes^[16]

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and exfoliated nanosheets from 3D frameworks (e.g., MOFs,^[17] COFs^[18] and zeolites^[19]), have enabled the design of high-performance separation membranes. By stacking these nanosheets, well-defined interlayer nanochannels were created, providing ultrafast water transport pathways while achieving molecular sieving. Moreover, the surface chemistry of these materials (e.g., charged terminations on MXenes) further enhances their selectivity *via* electrostatic interactions. Since their discovery in 2011, MXenes have been increasingly applied in environmental remediation. This is attributed to the remarkable and tunable physicochemical properties of MXenes, as well as their extremely short transport pathways and abundant nanochannels,^[20] which endow them with versatile surface functionality, high adsorption efficiency, larger specific surface area and excellent hydrophobicity.^[21] The unique advantages of MXenes make them ideal candidates for membrane separation materials. However, the poor flexibility prone to stacking and easy oxidation of pristine MXenes limit their practical applications.^[16] To address these issues, a composite strategy can be adopted by introducing flexible materials and isolating the surface coating. Consequently, MXene-polymer composite membranes have been extensively studied. Shen *et al.* incorporated u-Ti₃C₂T_x into a P84 polyimide matrix to fabricate a mixed-matrix membrane with optimized mass transport channels. The rejection rate of bromocyclohexane blue is maintained. In addition, charged MXenes can form electrostatic interactions with charged materials, making poly(ionic liquid) an ideal composite component.^[22]

In this study, two methods, layer-by-layer assembly and direct mixing, were employed to fabricate composite membranes by uniformly coating PCMVImTf₂N and MXene (Ti₂C) onto polypropylene (PP) membranes (Fig. 1). The influence of the preparation method and loading content on dye separation performance was systematically investigated. Methyl orange, methyl red, methylene blue, and rhodamine B were selected as the model dyes to study the retention performance of the as-prepared composite membranes. The effects of the precursor and dye concentrations on the composite membrane properties were systematically investigated. The re-

sults indicated that the SM-3 membrane exhibited excellent dye retention ratio and permeability, along with good cyclic stability. Symmetrical and asymmetric membranes have provided new research ideas for dye separation.

EXPERIMENTAL

Materials and Chemicals, Synthesis of Precursor, Characterizations

The details can be found in the electronic supplementary information (ESI).

Membrane Preparation

The AM-series composite membranes were fabricated *via* a layer-by-layer vacuum filtration method. Ti₂C powder was first dispersed in anhydrous ethanol with sonication for 0.5 h, and the dispersion was filtered onto a polypropylene (PP) substrate to form a uniform layer. The PILs powder was then dispersed separately in anhydrous ethanol under sonication for 0.5 h, followed by vacuum filtration onto a Ti₂C-modified substrate to obtain the final composite membrane.

The SM-series composite membranes were prepared *via* a one-step co-deposition method. The Ti₂C and PILs powders were mixed at the same mass ratio and co-dispersed in anhydrous ethanol with sonication for 0.5 h. The homogeneous mixed dispersion was vacuum-filtered directly onto a PP substrate to form a uniform composite membrane. The Ti₂C and PILs loading of the different composite membranes are listed in Table 1.

RESULTS AND DISCUSSION

To study the impact of different film formation methods on the final dye retention performance of membrane materials, we adopted two approaches to prepare membrane materials: the first involved dispersing a certain amount of Ti₂C powder, vacuum filtering, and then dispersing a certain amount of PILs powder evenly, followed by another filtration to obtain layer-stacked membrane materials, known as asymmetric membranes (AM); the second method involved evenly dispersing Ti₂C and PILs powders, and then filtering them in one step to form mem-

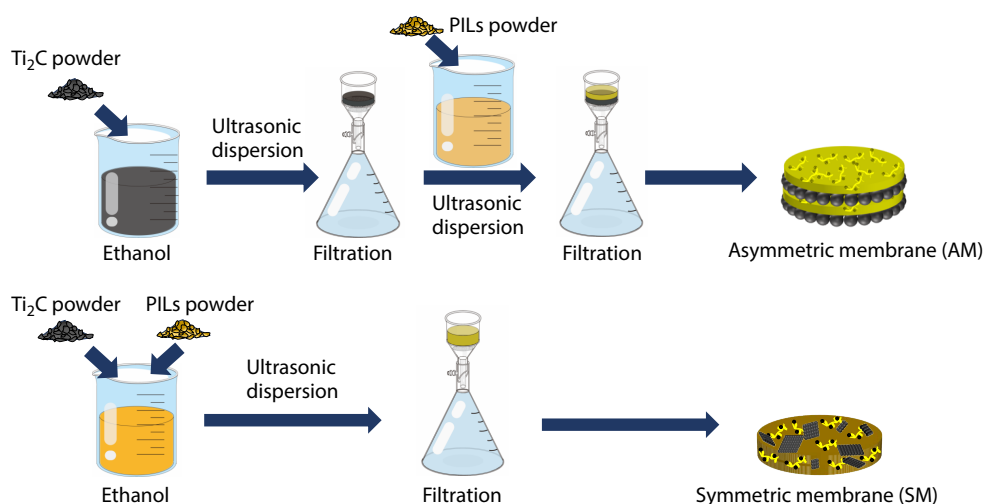


Fig. 1 The synthetic procedures for AM and SM.

Table 1 Ti₂C and PILs loading amounts of different membranes.

Membrane	Ti ₂ C content (mg)	PILs content (mg)
AM-1	3	3
AM-2	5	5
AM-3	7	7
SM-1	3	3
SM-2	5	5
SM-3	7	7

branes, known as symmetrical membranes (SM).

The ¹H-NMR spectrum of PCMVImTf₂N is shown in Fig. 2(A). The peak at 9.8 ppm corresponds to the proton connected to the positively charged nitrogen and another nitrogen atom on the imidazolium ring. The peaks at 8 ppm were numerous and complex, corresponding to the other two protons on the imidazolium ring. The peak at 5.5 ppm corresponds to methylene protons directly connected to the cyanide group and imidazolium ring. Peaks at 3.4 and 2.6 ppm are strong and prominent, representing protons on the polymer backbone. Peak at 3.4 ppm corresponds to the protons connected to the imidazolium ring, whereas the peak at 2.6 ppm corresponds to the methylene protons on the main chain.

Fig. 2(B) shows the X-ray diffraction (XRD) pattern of the MXene precursor. The XRD pattern of Ti₂C exhibited characteristic peaks at $2\theta=13.0^\circ$, 34.1° , and 60.8° , corresponding to its crystalline phase.^[23] The peak observed at approximately $2\theta=40^\circ$ was attributed to the partial oxidation of Ti₂C to TiO₂. From the XPS survey scanning (Fig. 2C) obtained on the sample surface in the vertical direction, we found that the sample mainly contained C, O, Ti and F. C and Ti should originate from the main structure of Ti₂C MXene, F should come from

the surface group of Ti₂C MXene or the residual reactants, and O is attributed to the partial oxidation of Ti₂C to TiO₂.

The FTIR spectra of Ti₂C, PILs, and SM-3 are presented in Fig. 2(D). In the PIL spectrum, the absorption band at 2210 cm⁻¹ was assigned to the cyanide group (CN) stretching vibration,^[24] while the band at 1187 cm⁻¹ is attributed to the symmetric stretching vibration of the imidazole ring.^[25] For Ti₂C, a strong and broad band at 3427 cm⁻¹ corresponds to the O—H stretching vibration,^[26] indicating the presence of hydroxyl (—OH) functional groups on the carbide surface post-preparation. Additionally, the band at 1714 cm⁻¹ is attributed to the characteristic C=O stretching vibration of the carboxyl (—COOH) groups.^[27] Notably, all functional groups of the two substances were observed in the spectrum of SM-3. Thus, FTIR analysis not only confirmed the successful synthesis of Ti₂C and PILs but also verified the fabrication of the composite membrane.

The static contact angle, which decreases as the solid surface tension increases, serves as an indicator of the hydrophilicity or hydrophobicity of the membrane surface.^[28] The static contact angles of the asymmetric and symmetric membranes are shown in Figs. 2(E) and 2(F). The water static contact angles on the surfaces of the asymmetric and symmetric membranes were 87.00° and 45.50°, respectively. The larger contact angle for the asymmetric membranes is due to the more hydrophobic PILs positioned on the surface during preparation. In contrast, in the preparation of symmetric membranes, the less dense and more hydrophilic Ti₂C powder ends up relatively on top, resulting in a smaller contact angle. This result was consistent the expected outcome.

Scanning electron microscopy (SEM) images (Fig. 3a)

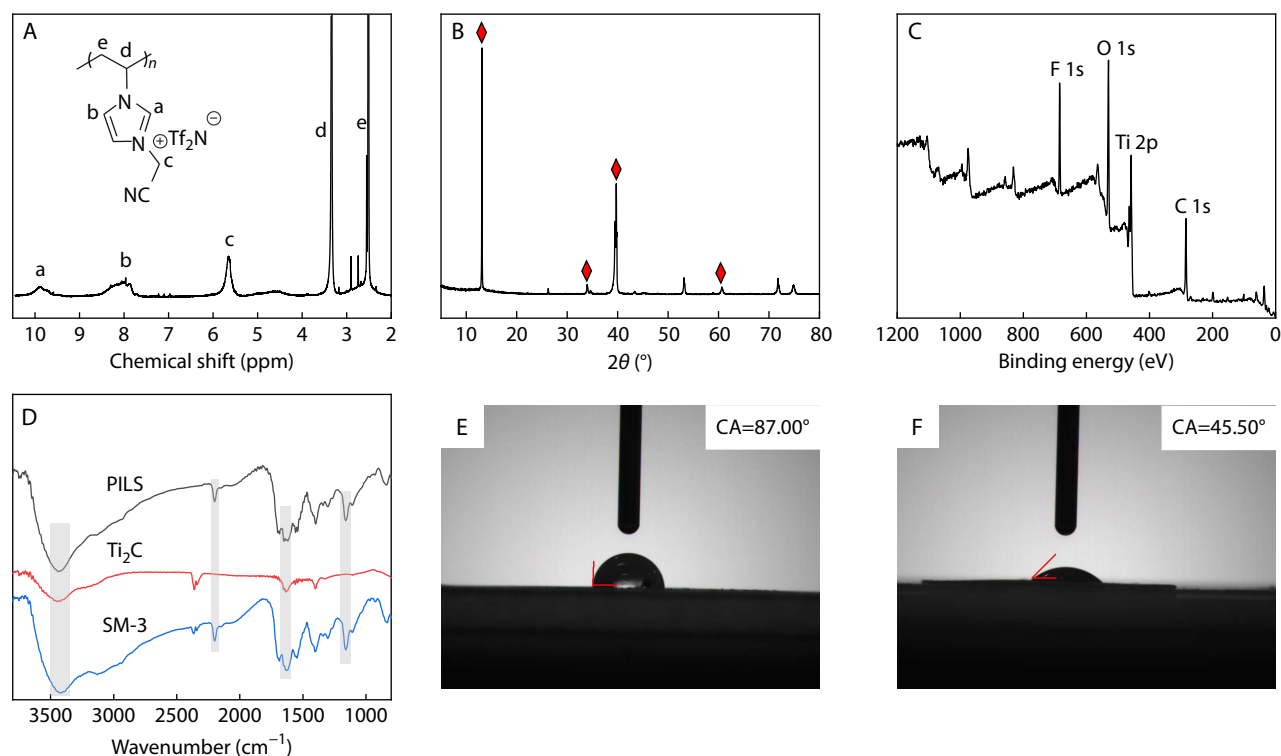


Fig. 2 (A) The ¹H-NMR spectrum of PCMVImTf₂N; (B) XRD pattern of the Ti₂C; (C) The XPS survey scanning of Ti₂C; (D) The FTIR spectra corresponding to Ti₂C, PILs and SM-3; The static contact angles of (E) the asymmetric membrane and (F) symmetric membrane.

showed that the poly(ionic liquid)s consisted of numerous irregularly shaped and unevenly sized small particles, closely packed into larger particles, while the larger particles were sparsely distributed. From SEM image (Fig. 3b) of Ti_2C , typical multilayer features of Ti_2CT_x MXene were observed after treatment with HCl and LiF,^[29] characterized by multiple MXene layers bound by weak van der Waals forces rather than single-layer MXene structures.^[30] F^- and hydroxyl etching removes the Al layer, and the water-based etching medium provides hydrophilicity, making MXene an excellent candidate for polymer composites. The presence of numerous irregular PILs particles on the AM membrane surfaces is apparent from Fig. 3(c) because of the positioning of PILs in the upper layer during membrane material preparation. SM membrane images (Fig. 3d) show the presence of multilayer Ti_2C sheet structures, due to less dense Ti_2C occurring in the upper layer during the preparation process. The cross-sectional SEM image (Fig. 3e) shows granular PILs covering the surface with an evident lamellar structure underneath. The layered morphology is consistent with the characteristics of asymmetric membranes. In the cross-sectional SEM image (Fig. 3f) of AM, granular PILs and lamellar MXene are uniformly dispersed, presenting the typical morphology of symmetric membranes. The SEM of the membranes corroborate the contact angle measurements. To investigate the structural evolution induced by different PILs/ Ti_2C loadings, the cross-sectional morphologies of the AM-1, AM-2, and AM-3 membranes were characterized using cross-sectional SEM. As shown in Figs. 3(g)–3(i), all membranes exhibit a typical asymmetric struc-

ture. The results indicated that the membrane thickness increased progressively with increasing loading. Specifically, the thicknesses of the AM-1, AM-2, and AM-3 membranes were determined to be 61.14, 67.93, and 79.16 μm , respectively. This gradual increase in thickness is consistent with the accumulation of the PILs/ Ti_2C selective layer, implying an increase in the effective transport path length for water molecules.

Based on the dye separation performance experimental results shown in Figs. 4(a)–4(e) and Table 2, the areal loading of the membrane material significantly affects both the permeability and dye rejection performance; notably, increased permeability is often accompanied by reduced rejection capacity. The permeabilities of AM-1 and SM-1 membranes reached 229.30 and 382.17 $\text{L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{MPa}^{-1}$, respectively, representing relatively high levels compared to similar types of membranes reported in the literature. However, their dye rejection performance was notably poor, particularly for the SM-1 membrane, which exhibited a rejection rate of only 20.9% for methylene blue. As the areal loading gradually increased, the permeability decreased whereas the rejection rate improved substantially. Compared with other reported high-performance composite membranes for dye separation (Table 3), this work achieved a water flux of 125.86 $\text{L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{MPa}^{-1}$ while maintaining a high dye rejection rate, which is significantly higher than those in previous studies. Furthermore, a comparative analysis between AMs and SMs revealed that the SMs offer superior permeability, whereas the AMs demonstrated higher dye rejection. The enhanced permeability of

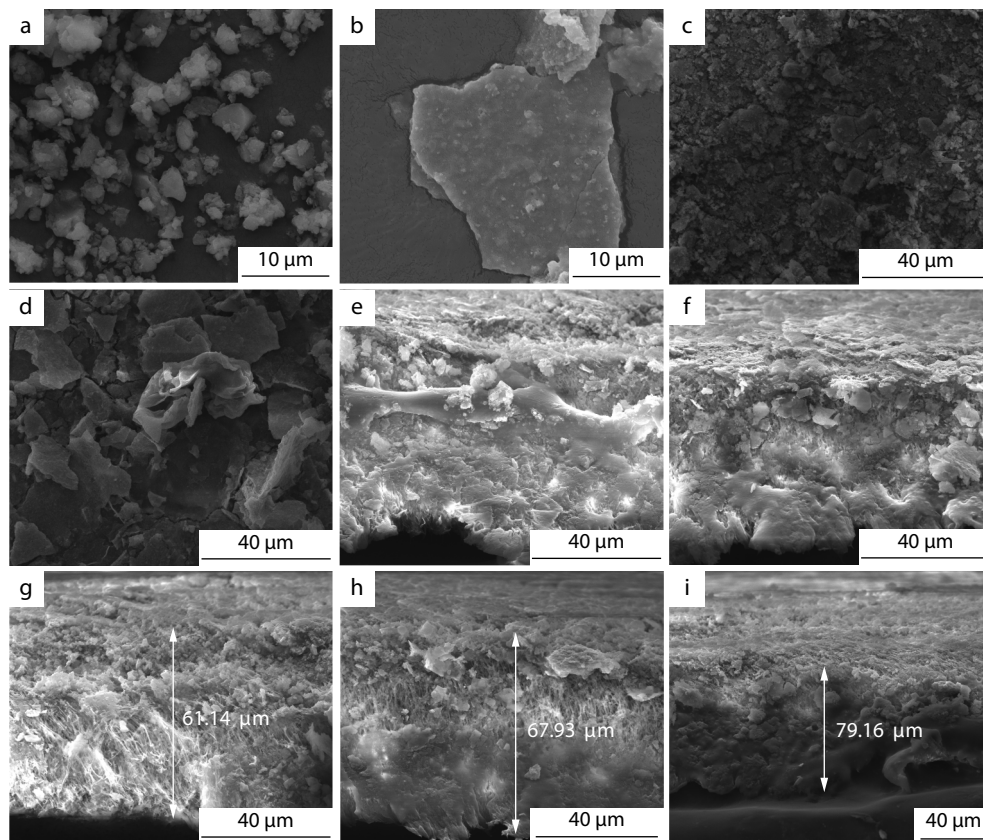


Fig. 3 Surface SEM images of (a) PILs, (b) Ti_2C , (c) AM, (d) SM and cross-sectional SEM images of (e) AM, (f) SM, (g) AM-1, (h) AM-2 and (i) AM-3.

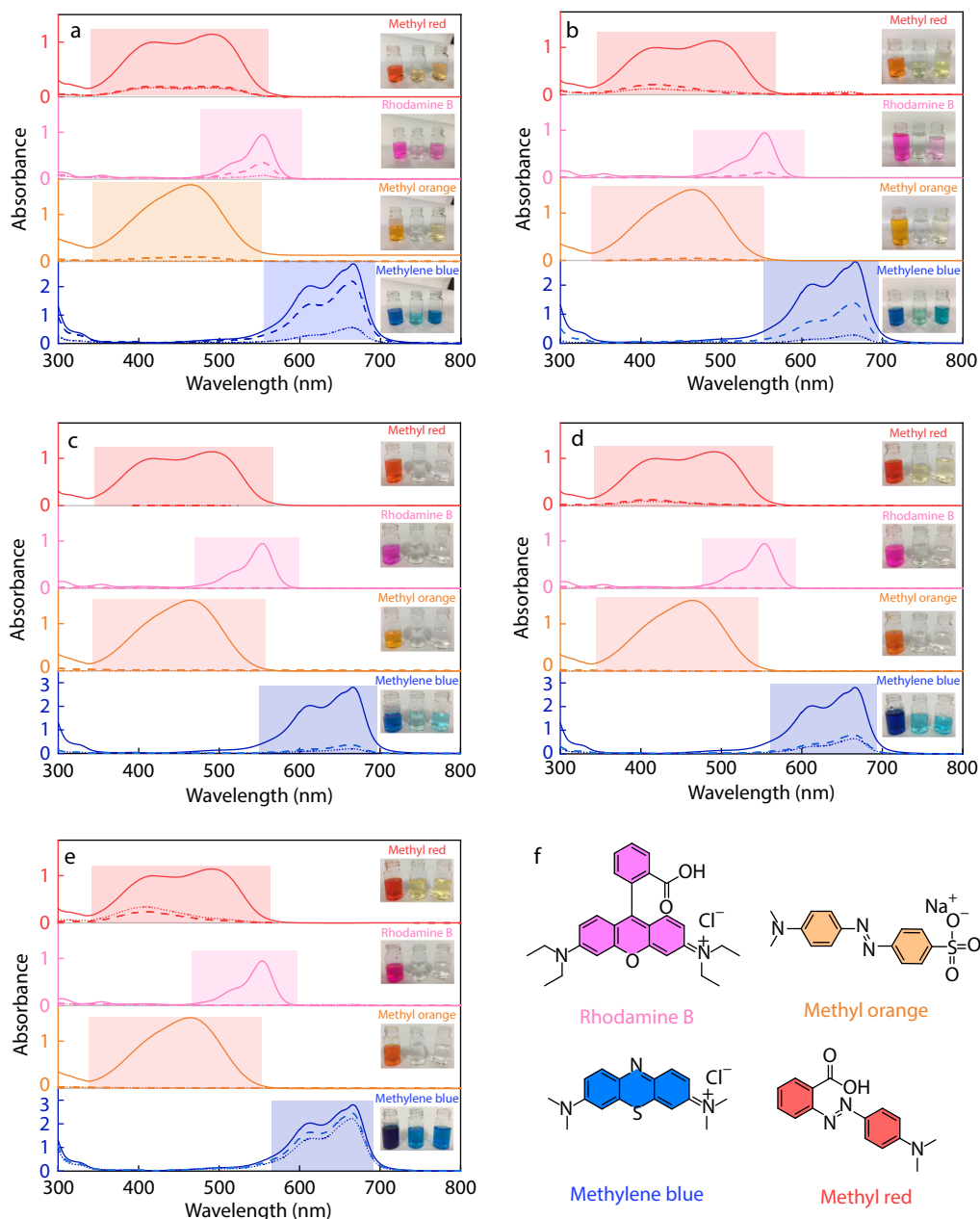


Fig. 4 UV spectra of dye retention test of membrane (a) AM-1 and SM-1, (b) AM-2 and SM-2, (c) AM-3 and SM-3 with dye concentration: $20 \text{ mg}\cdot\text{L}^{-1}$, (d) AM-3 and SM-3 with dye concentration: $60 \text{ mg}\cdot\text{L}^{-1}$, (e) AM-3 and SM-3 with dye concentration: $100 \text{ mg}\cdot\text{L}^{-1}$ (The solid line, dashed line, and dotted line represent origin solvent, SM and AM); (f) Molecular formulas of four dyes.

Table 2 Permeability and dye retention of various membranes.

Membrane	Dye concentration ($\text{mg}\cdot\text{L}^{-1}$)	Permeability ($\text{L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{MPa}^{-1}$)	Rejection ratio (%)			
			Rhodamine B	Methyl orange	Methylene blue	Methyl red
AM-1	20	229.30	92.1	99.5	80.1	83.2
SM-1	20	382.17	63.0	93.5	20.9	81.0
AM-2	20	125.86	99.5	99.8	90.0	87.5
SM-2	20	186.00	87.7	97.2	50.4	78.3
AM-3	20	47.77	>99.9	>99.9	92.8	>99.9
SM-3	20	58.36	>99.9	>99.9	87.0	99.6
AM-3	60	47.77	>99.9	>99.9	92.4	98.0
SM-3	60	58.36	>99.9	>99.9	90.5	96.1
AM-3	100	47.77	>99.9	>99.9	84.2	95.5
SM-3	100	58.36	>99.9	>99.9	82.5	93.6

Table 3 The reported composite membranes for dye separation.

Membrane	Permeability ($\text{L}\cdot\text{m}^{-2}\cdot\text{h}^{-1}\cdot\text{MPa}^{-1}$)	Rejection ratio (%)	Ref.
SiO_2 -PIL	189.23	Reactive black 5: 90 Reactive red 49: 85	[31]
PIL-PVDF	0.834	Acid red: 98.6 Methyl orange: 81.8 Crystal violet: 99.6 Rhodamine B: 88.3	[14]
PIL-MOF-808-PVDF	5.808	Congo red: 97.6	[32]
PIL- TiO_2 -PSF	128.56	Methyl blue: 90.83 Congo red: 94.28 Evan's blue: 65.89 Methyl orange: 30.98	[33]
MXene($\text{Ti}_3\text{C}_2\text{T}_x$)-COFs	about 30	Congo red: 98.2 Chrome black T: 98.7 Methyl blue: 96.4 Methyl orange: 97.2	[18]
MXene ($\text{Ti}_3\text{C}_2\text{T}_x$)-ANF	19.53	Alcian blue: 99.1 Congo red: 96.1 Rose bengal: 98.6	[34]
Mxene-AgNW	5.13	Methyl orange: 99.2	[35]
Mxene($\text{Ti}_3\text{C}_2\text{T}_x$)-PIL	9.78	Congo red: 99.0	[36]
This work	125.86	Rhodamine B: 99.5 Methyl orange: 99.8 Methylene blue: 90.0 Methyl red: 87.5	/

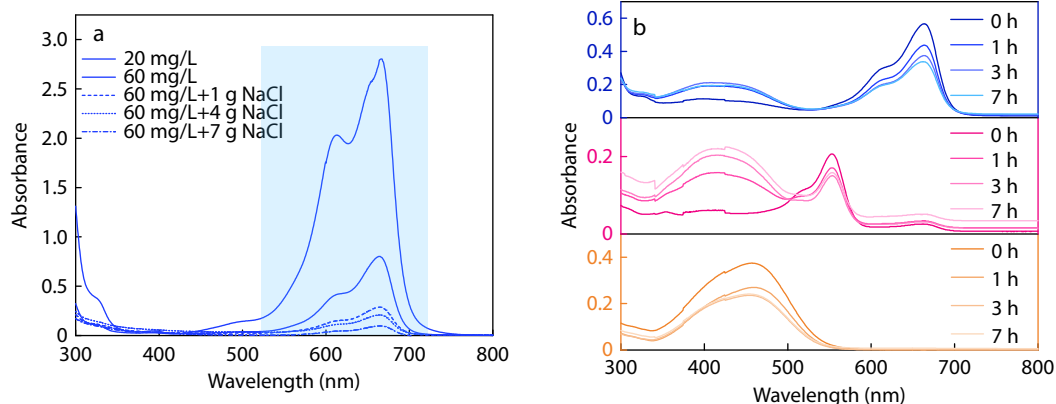
SMs is attributed to the uniform mixing of PILs and Ti_2C , where Ti_2C nanosheets are randomly interspersed between the PIL particles, providing more separation channels than in composite structures. Importantly, the membrane rejection performance toward methylene blue was markedly weaker than those of the other tested dyes. Consequently, we further investigated the underlying rejection mechanisms.

The primary factors affecting dye rejection can be broadly classified into two categories: electrostatic repulsion or attraction of charged membranes and the size of the dye molecule.^[37,38]

The molecular structures of the four dyes (Methyl orange, Methyl red, Methylene blue and Rhodamine B) are illustrated^[39–42] in Fig. 4(f). However, the rejection of individual dye molecules through membrane pores is not solely governed by their molecular size, as dyes predominantly exist as aggregates.^[43] The aggregation state is influenced by factors such as the inherent properties of the dye, concentration, pH, temperature, and electrolyte content. To elucidate the poor rejection of Methylene blue by the SM-3 membrane, two ex-

perimental approaches were designed. The electrolyte concentration was selected as the controllable variable to evaluate the effect of aggregation size as inorganic salt ions compete for solvating water to lower dye solubility and compress the electrical double layer, which weakens the electrostatic repulsion between dye molecules and induces their transition from stable dispersion to aggregation.^[44–47] Three 100 mL of solutions of Methylene blue (60 mg/L) were prepared, supplemented with 1, 4, and 7 g of strong electrolyte NaCl. After filtration through the SM-3 membrane, UV-Vis spectroscopy was performed. The results showed that the membrane rejection rate for Methylene blue increased proportionally with the NaCl concentration (Fig. 5a). This experiment confirmed that the aggregate size critically governs the rejection efficiency.

To evaluate the impact of the membrane surface charge on rejection, three 10 mL aliquots of dye solutions (5 mg/L each) were prepared. Identical SM-3 membrane samples (equal in size and weight) were added, and UV-Vis measurements were taken at 1, 3 and 7 h. The results indicated that the positively



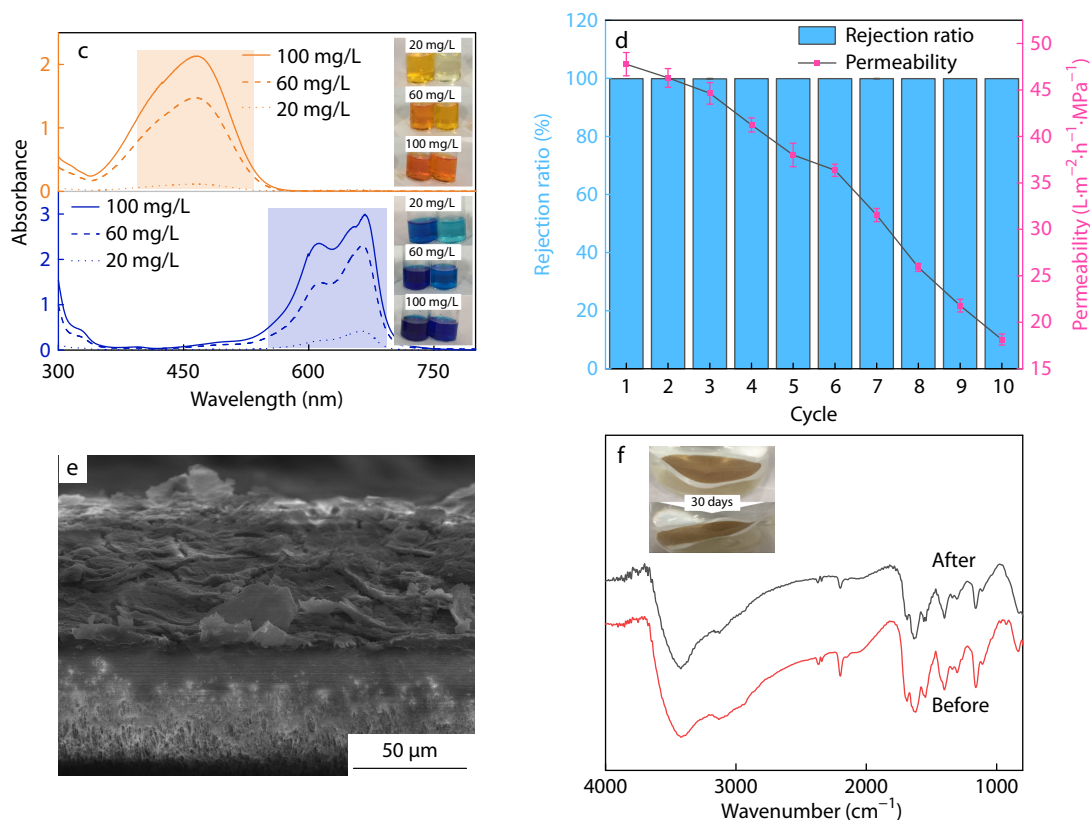


Fig. 5 (a) Effect of electrolyte concentration on methylene blue rejection performance; (b) Dye adsorption at different soaking times; (c) UV spectra of dye retention test for negatively charged SM-3 membrane; (d) Diagram of membrane cyclic performance test; (e) Cross-sectional SEM image of SM-3 after cycling; (f) The FTIR spectra of the membrane before and after soaking.

Table 4 Comparison of dye retention of positively and negatively charged SM-3 membranes.

Membrane	Dye concentration (mg·L ⁻¹)	Permeability (L·m ⁻² ·h ⁻¹ ·MPa ⁻¹)	Rejection ratio (%)	
			MO	MB
Positively charged	20	57.68	>99.9	87.0
	60		>99.9	90.5
	100		>99.9	92.5
Negatively charged	20	43.24	92.0	85.6
	60		66.3	73.4
	100		43.8	44.5

charged membrane exhibited slightly stronger adsorption for the anionic dye Methyl orange (MO) than for the cationic dye Methylene blue (MB) (Fig. 5b). This indicates that the surface charge from nitrogen or other heterocycles significantly influences the rejection performance. For MO, cationic adsorption may hinder permeation. To validate this, PILs and poly(acrylic acid) (PAA) powders were blended at specific ratios, dispersed in NMP solution, and stirred for 1 h. Electrostatic crosslinking occurred between positively charged PILs and negatively charged PAA chains.^[48] At higher PAA content, the membrane surface was modified to a negatively charged state. Rejection tests against MO and MB solutions showed that after becoming negatively charged, the membrane exhibited smaller changes in the MB rejection rate than MO (Fig. 5c and Table 4), further confirming the critical role of electrostatic interactions in dye separation. In contrast to Methyl orange, Methyl red and Rhodamine B, Methylene blue consistently exhibited a lower rejection rate across all the mem-

brane samples. This phenomenon cannot be solely explained by the molecular size effect, since Methyl orange possesses a smaller molecular dimension than MB, yet shows a much higher rejection. Instead, the surface charge of the membrane played a dominant role. Our membrane is positively charged under the experimental conditions shown in Fig. 5(c), which shows that the membrane has stronger adsorption toward the anionic dye Methyl orange. The electrostatic repulsion between the positively charged membrane surface and cationic MB molecules is considerably weak, which reduces the energy barrier for MB to pass through the membrane nanochannels. In contrast, the strong electrostatic attraction between the positively charged membrane and anionic methyl orange significantly enhanced its retention. This interpretation is strongly corroborated by the charge-reversal experiments in Table 4. When the membrane was converted to a negatively charged state, the rejection of anionic MO dropped sharply, while the rejection of cationic MB de-

creased only moderately. Additionally, as shown in Fig. 5(a), the rejection of MB can be substantially improved by inducing dye aggregation through the addition of NaCl, indicating that the smaller aggregate size of MB under normal conditions contributes to its higher permeability. Therefore, the relatively low rejection of MB arises from the combined effect of weak electrostatic repulsion and the small effective aggregate size. In summary, the electrostatic repulsion or attraction of charged membranes and the size of the dye molecules can affect both the permeability and rejection capacity of the membrane material. However, the specific extent of their impact depends on particular conditions.

To test the recycling performance of the membranes, the SM-3 membranes were repeatedly tested for permeability and retention using 60 mg·L⁻¹ of Methyl orange solutions for 10 cycles. The results are showed in Fig. 5(d). The membrane retention of Methyl orange remained above 99%, while permeability declined from 47.77 L·m⁻²·h⁻¹·MPa⁻¹ to 18.15 L·m⁻²·h⁻¹·MPa⁻¹.

Although the flux declined, the final stabilized flux remained at a relatively high level compared with similar membrane studies treating dye-containing wastewater (Table 3).

This suggests that the membrane developed in this study possesses certain advantages in terms of fouling resistance and long-term flux maintenance. Cross-sectional SEM image (Fig. 5e) of the membrane after cycling that its structure became denser than before cycling. Therefore, the observed decline in permeability is likely attributable to pore blockage caused by dye accumulation.

Similarly, to study the stability of the membranes during use, the complete membrane materials were immersed in tap water for 30 days. As shown in The FTIR spectra (Fig. 5f) of the membrane before and after soaking, the characteristic peaks of the membrane before and after soaking remained almost identical, with no significant shifts or appearance/disappearance of peaks. To further demonstrate the structural integrity of the membrane, the separation performance of the SM-3 membrane was re-evaluated after 30 days of immersion in an aqueous solution. As summarized in Table 5, the membranes exhibit excellent separation capabilities. These results confirmed that the chemical structure and selective separation channels of the SM-3 membrane were not compromised during long-term immersion, validating its robust structural stability for practical applications.

Table 5 Separation performance of SM-3 before and after soaking in aqueous solution.

Membrane	Dye concentration (mg·L ⁻¹)	Permeability (L·m ⁻² ·h ⁻¹ ·MPa ⁻¹)	Rejection ratio (%)			
			Rhodamine B	Methyl orange	Methylene blue	Methyl red
SM-3 (Before)	20	58.36	>99.9	>99.9	87.0	99.6
SM-3 (After)	20	55.72	>99.9	>99.9	88.4	99.2

CONCLUSIONS

In this study, PILs/MXene composite membranes with tunable asymmetric and symmetric structures were successfully developed on commercial PP substrate membranes. The strategic integration of PILs with MXene synergistically resolves the inter-layer stacking issue of neat MXene and the instability of pure PILs, thereby effectively showing separation performance for Methyl orange, Methyl red, Methylene blue, and Rhodamine B. Benefiting from the size exclusion of MXene nanochannels and the electrostatic repulsion of PILs, the optimized membranes achieved superior dye rejection rates at higher loading levels (e.g., AM-3/SM-3) while maintaining a high water flux (up to 58.36 L·m⁻²·h⁻¹·MPa⁻¹). The facile coating strategy combined with the use of cost-effective commercial materials, offers a potential pathway for industrial scale-up. The stability of the membranes further underscores their practical viability for long-term operation in complex industrial dye wastewater treatment, providing a scalable and efficient solution for environmental remediation.

Conflict of Interests

The authors declare no interest conflict.



Electronic Supplementary Information

Electronic supplementary information (ESI) is available free of

charge in the online version of this article at <http://doi.org/10.1007/s10118-026-3800-9>.

Data Availability Statement

The related data (DOI: 10.57760/sciencedb.j00189.00070) for this work is available in the Data Repository of China Association for Science and Technology database (<https://www.scidb.cn/c/cjps>), and the software for opening the data is Origin.

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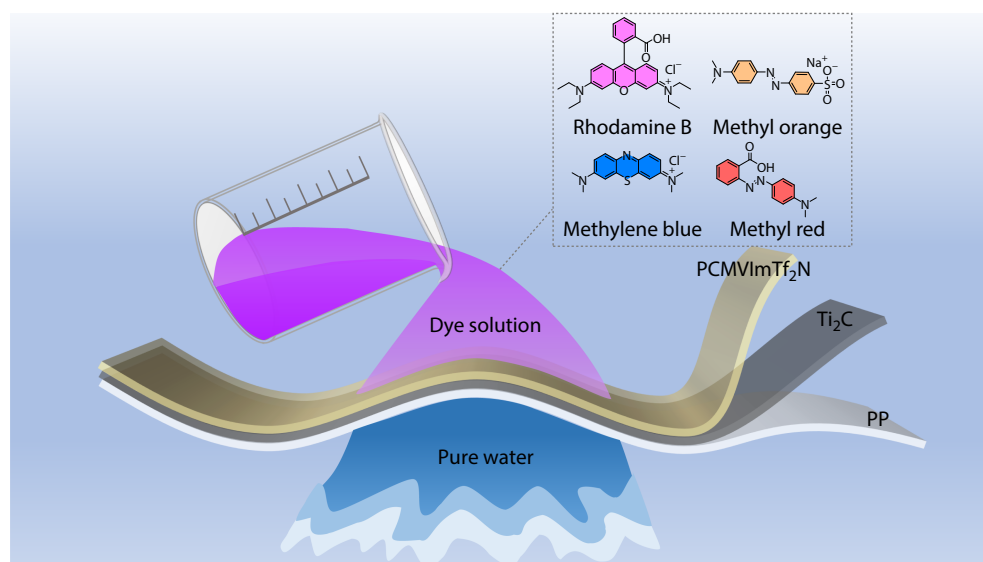
Graphical Abstract

Nitrogen-enriched Heterocyclic Poly(ionic liquid)s/MXene Composite Membranes for Efficient Dye Separation

Jiang Li, Jun-Tao Tang, Chun Tian, Shuai Gu, Peng-Peng Shao, Rui-Ren Tang, Chen-Xiang Ai, and Gui-Peng Yu

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In this study, PCMVImTf₂N/Ti₂C composite membranes were used to achieve efficient dye separation. The membranes at higher loading levels exhibited retention rates for four dyes: Rhodamine B, Methyl orange, Methylene blue, and Methyl red, while maintaining a high water flux.



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